UNIFIED FACILITIES CRITERIA (UFC)

DESIGN: ENGINEERING WEATHER DATA

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U.S. ARMY CORPS OF ENGINEERS

NAVAL FACILITIES ENGINEERING COMMAND (Preparing Activity)

AIR FORCE CIVIL ENGINEER CENTER

Record of Changes (changes are indicated by \1\ ... /1/)

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This UFC supersedes UFC 3-400-02, dated February 2003.
FOREWORD

The Unified Facilities Criteria (UFC) system is prescribed by MIL-STD 3007 and provides planning, design, construction, sustainment, restoration, and modernization criteria, and applies to the Military Departments, the Defense Agencies, and the DoD Field Activities in accordance with USD (AT&L) Memorandum dated 29 May 2002. UFC will be used for all DoD projects and work for other customers where appropriate. All construction outside of the United States is also governed by Status of Forces Agreements (SOFA), Host Nation Funded Construction Agreements (HNFA), and in some instances, Bilateral Infrastructure Agreements (BIA.) Therefore, the acquisition team must ensure compliance with the most stringent of the UFC, the SOFA, the HNFA, and the BIA, as applicable.

UFC are living documents and will be periodically reviewed, updated, and made available to users as part of the Services’ responsibility for providing technical criteria for military construction. Headquarters, U.S. Army Corps of Engineers (HQUSACE), Naval Facilities Engineering Command (NAVFAC), and Air Force Civil Engineer Center (AFCEC) are responsible for administration of the UFC system. Defense agencies should contact the preparing service for document interpretation and improvements. Technical content of UFC is the responsibility of the cognizant DoD working group. Recommended changes with supporting rationale should be sent to the respective service proponent office by the following electronic form: Criteria Change Request. The form is also accessible from the Internet sites listed below.

UFC are effective upon issuance and are distributed only in electronic media from the following source: Whole Building Design Guide web site http://dod.wbdg.org/.

Refer to UFC 1-200-01, DoD Building Code (General Building Requirements), for implementation of new issuances on projects.

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UNIFIED FACILITIES CRITERIA (UFC)  
REVISION SUMMARY SHEET

Document: UFC 3-400-02, DESIGN: ENGINEERING WEATHER DATA

Superseding: UFC 3-400-02, dated 28 February 2003

Description: The purpose of this document is to provide an overview of and instructions for access to climate data available for use by engineers designing government structures. Final selection of sites was based upon availability of climate data. Most are located at military installations supporting airfield operations, or at local airports/airfields. This UFC is applicable to all service elements and contractors involved in the planning, design and construction of DoD facilities worldwide.

Reasons for Document:
- To update document to include new procedures for accessing weather data, new selection sites, new design values and new format.

Impact:
- There are no impacts.

Unification Issues
None.
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CHAPTER 1 INTRODUCTION

1-1 PURPOSE AND SCOPE.

The purpose of this document is to provide an overview of and instructions for access to climate data available for use by engineers designing government structures.

The 14th Weather Squadron (14 WS), formerly AFCCC, compiled Engineering Weather Data (EWD) at the request of the Air Force Civil Engineering Center (AFCEC). Sites were identified by AFCEC, US Army Corps of Engineers (USACE), and the Naval Facilities Engineering Command (NAVFAC). Final selection of sites was based upon availability of climate data. Most are located at military installations supporting airfield operations, or at local airports/airfields. Non-DoD requests may be satisfied from a private consulting meteorologist or from NOAA's National Centers for Environmental Information (NCEI, formally the National Climatic Data Center). Each site's EWD is presented as a PDF. To comply with Standard 90.1-2013, Energy Standard for Buildings Except Low-Rise Residential Buildings, co-sponsored by the American Society of Heating, Refrigerating, and Air Conditioning Engineers and the Illuminating Engineering Society of North America (ASHRAE/IESNA) and approved by the American National Standards Institute (ANSI), the 14 WS has added a separate comma separated values file containing all cooling degree-day data based on 50°F for all sites. Paragraph in Chapter 2 entitled “Alternate Cooling Degree-Days Calculation” covers the use of this file in more detail. Bin Temperature Data .csv files are suitable for importing into Microsoft® Excel.

1-2 APPLICABILITY.

This UFC is applicable to all service elements and contractors involved in the planning, design and construction of DoD facilities worldwide.

1-3 GENERAL BUILDING REQUIREMENTS.

Comply with UFC 1-200-01, DoD Building Code (General Building Requirements). UFC 1-200-01 provides applicability of model building codes and government unique criteria for typical design disciplines and building systems, as well as for accessibility, antiterrorism, security, high performance and sustainability requirements, and safety. Use this UFC in addition to UFC 1-200-01 and the UFCs and government criteria referenced therein.

1-4 REFERENCES.

Appendix A contains a list of references used in this document. The publication date of the code or standard is not included in this document. Unless otherwise specified, the most recent edition of the referenced publication applies.

1-5 GLOSSARY.
Appendix C contains acronyms, abbreviations, and terms.

1-6 ACCESSING EWD.

1-6.1 Retrieving data for .mil domain users.


2. A Common Access Card (CAC) is required to access the 14th Weather Squadron’s web site. If you do not have one, call 828-271-4291 to request an EWD or send an email request to 14WS_SAR@us.af.mil.

3. A CAC user can also electronically submit a Support Assistance Request by clicking on the “Request Support” tab at the top of the 14 WS website.

1-6.2 Retrieving Data for Non-DoD (non CAC) Users.

Non-DoD users (e.g., contractors) may access data from the 14 WS if they are working on a DoD contract. If so, follow these instructions:

1. Fill out the Sample SAR Form in Appendix D, and send an email requesting support to 14WS_SAR@us.af.mil. This email inbox is monitored Monday –Friday 0730-1630 with the exception of holidays.

2. Pay particular attention to the fields requesting a complete description of the information being requested (e.g., site location and coordinates), a suspense date, a statement about how the data applies to the mission and the contract number.

3. The 14 WS must be able to verify that the contractor is working on a valid DoD contract before providing the information. The 14 WS will then e-mail the appropriate PDF file for the site requested. Non-DoD contractors and vendors must contact the National Centers for Environmental Information (NCEI, formally NCDC) to purchase the Engineering Weather Data (EWD).

4. Retrieving data for unlisted sites. If a station is not in the EWD list, fill out the 14 WS Support Assistance Request (SAR) form (example in Appendix D) and pay particular attention to the fields requesting a complete description of the information being requested (e.g., site location and coordinates), a suspense date, a statement about how the data applies to the mission, and the contract number.
CHAPTER 2 DATA DESCRIPTION AND APPLICATIONS

2-1 INTRODUCTION.

This chapter summarizes each page in a typical site data set and provides guidance for using the data.

2-2 DATA SET PAGE 1: CLIMATE SUMMARY.

Figure 2-1 is a sample of Data Set Page 1, which summarizes the site’s climate.

2-2.1 Location Information.

This section of Data Set Page 1 contains a summary table that includes site name, location, elevation (above mean sea level), period of record (POR), and average (atmospheric) pressure not corrected to sea level (higher elevations result in lower pressures). The POR is the time frame over which the data used to compute the statistics in this document were compiled.

2-2.2 Design Values.

2-2.2.1 Explanation of Design Values.

Design values are provided for dry bulb temperature, wet bulb temperature, and humidity ratio at specific percentile frequencies of occurrence. The design values of 0.4%, 1%, and 2% are based on the entire year. The winter design values of 99.6%, 99%, and 97.5% are also based on the entire year. In other words, the design values are annual values, not seasonal values. These design values were instituted for several reasons. At some locations, the warmest or coldest months of the year do not fall into the months listed above. It is easier to compare locations that are in tropical or marine climates where there is less seasonal variability. It is also more straightforward to compare southern hemisphere locations.
### Sample Data Set

**SCOTT AFB MIDAMERIC**

- Latitude = 38.55 N
- Longitude = 89.84 W
- Period of Record = 1985 To 2014
- Station ID = ICAO KBLV
- Elevation = 459 Feet
- Average Pressure = 29.55 inches Hg

<table>
<thead>
<tr>
<th>Dry Bulb Temperature (T)</th>
<th>Mean Coincident (Average) Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Design Value (°F)</td>
<td>Wet Bulb Temperature (°F)</td>
</tr>
<tr>
<td>--------------------------</td>
<td>--------------------------</td>
</tr>
<tr>
<td>Median of Extreme Highs</td>
<td>100</td>
</tr>
<tr>
<td>0.4% Occurrence</td>
<td>95</td>
</tr>
<tr>
<td>1.0% Occurrence</td>
<td>93</td>
</tr>
<tr>
<td>2.0% Occurrence</td>
<td>90</td>
</tr>
<tr>
<td>Mean Daily Range</td>
<td>20</td>
</tr>
<tr>
<td>97.5% Occurrence</td>
<td>18</td>
</tr>
<tr>
<td>99.0% Occurrence</td>
<td>11</td>
</tr>
<tr>
<td>99.6% Occurrence</td>
<td>7</td>
</tr>
<tr>
<td>Median of Extreme Lows</td>
<td>0</td>
</tr>
</tbody>
</table>
2-2.2.2  Dry Bulb Temperature.

2-2.2.2.1  Median of Extreme Highs (or Lows).

The dry bulb temperature extreme high (or low) is determined for each calendar year of the POR along with the coincident values for wet bulb temperature, humidity ratio, wind speed, and prevailing wind direction. Median values are determined from the distribution of extreme highs (or lows).

2-2.2.2.2  0.4%, 1.0%, 2.0%, 97.5%, 99.0%, and 99.6% Dry Bulb Design Values.

Listed is the dry bulb temperature corresponding to a given annual cumulative frequency of occurrence and its respective mean coincident values for wet bulb temperature, humidity ratio, wind speed, and prevailing wind direction. The dry bulb temperature listed represents the value that was exceeded for the respective percent of time over the entire POR. For example, the 1.0% occurrence design value temperature (92 °F) has been exceeded only 1 percent of the time during the entire POR. All the observations occurring within one degree of the design value are grouped, and the
Mean Coincident (Average) Values for Wet Bulb Temperature, Humidity Ratio, and Wind Speed are calculated. The prevailing wind direction (the “mode” of the wind direction distribution) is also calculated.

2-2.2.2.3 Mean Daily Range.

The mean daily range (difference between daily maximum and daily minimum temperatures) is the average of all daily dry bulb temperature ranges for the POR.

2-2.3 Wet Bulb Temperature.

2-2.3.1 Median of Extreme Highs.

The Median of Extreme Highs value for wet bulb temperature is the highest annual extreme wet bulb temperature averaged over the POR. The corresponding Mean Coincident (Average) Values are determined the same way as for the respective values for dry bulb temperature.

2-2.3.2 0.4%, 1.0 %, 2.0% Wet Bulb Temperature Design Values.

The design values listed and the corresponding Mean Coincident (Average) Values are determined the same way as for dry bulb temperature, described in 2-2.2.2.2.

2-2.4 Humidity Ratio.

2-2.4.1 Median of Extreme Highs.

The value for humidity ratio is the highest annual extreme averaged over the POR. The corresponding Mean Coincident (Average) Values are determined the same way as described in 2-2.2.2.2.

2-2.4.2 0.4%, 1.0%, and 2.0% Humidity Ratio Design Values.

Design values are provided for humidity ratio and the corresponding Mean Coincident (Average) Values for dry bulb temperature, vapor pressure, wind speed, and wind prevailing direction.

2-2.5 Air Conditioning/Humid Area Criteria.

These are the number of hours, on average, that dry bulb temperatures of 34 °C (93 °F) and 27 °C (80 °F) and wet bulb temperatures of 23 °C (73 °F) and 19 °C (67 °F) are equaled or exceeded during the year.

2-2.6 Other Site Data.

This information is provided for general reference only, and should not be used as the basis for design. There are some locations for which this data is not available. In these cases, that portion of the table will be left blank.

2-2.6.1 Weather Region.
Eleven weather regions have been developed by the Department of Energy. They are defined by the range of cooling-degree days and heating-degree days based on 65 °F. ASHRAE/IESNA Standard 90.1 of 2001 uses annual HDD65 (Heating Degree Days based on 65 °F) and CDD50 (Cooling Degree Days based on 50 °F) to select the appropriate Building Envelope Requirements table for energy conservation design. Refer to paragraph 2-10 for further explanation of this data.

2-2.6.2 Ventilation Cooling Load Index.

The Ventilation Cooling Load Index (VCLI) is a two-part index that defines the total annual cooling load for ventilation air by calculating sensible heat load separately from the latent heat load (moisture). The results are expressed in ton-hours per cubic feet per minute per year of latent and sensible load. Values for sensible heat load are calculated by comparing the outdoor temperature to indoor conditions (75 °F and 60% relative humidity [RH]), and calculating how much energy is required to bring the outdoor air to the indoor temperature. The latent load is calculated similarly. Separate calculations are made for each hour of the year and then summed to form the annual VCLI.

2-2.6.3 Average Annual Freeze-Thaw Cycles.

This value is the average number of times per year that the air temperature first drops below freezing and then rises above freezing, regardless of the duration of either the freezing or thawing. The number of cycles is summed per year and averaged over the entire POR. Days with high temperatures or low temperatures at 0 °C (32 °F) are not counted for a freeze-thaw cycle. A cycle is counted only when the temperature drops below freezing (-0.5 °C [31 °F] or colder) or goes above freezing (0.5 °C [33 °F] or warmer).

2-2.6.4 Other Values.

The following values are derived from sources other than the 14 WS. Engineers and architects should review the publications listed below and contact the organizations for current values, including background information and complete guidelines for use of these data elements.

2-2.6.4.1 Groundwater.

National Ground Water Research and Educational Foundation
601 Dempsey Road
Westerville OH 43081-8978
(800) 551-7379
http://www.ngwa.org/

NOTE: Average groundwater temperature parallels long-term average air temperature, because soil at a depth of 15 meters (50 feet) does not undergo significant temperature change over the course of a year. Soil temperature at 15 meters stays slightly warmer than average annual air temperature by approximately 1.4 °C (2.5 °F).

2-2.6.4.2 Rain Rate.
2-2.6.4.3 Frost Depth, Basic Wind Speed, Ground Snow Loads.

ANSI/ASCE 7-95, Minimum Design Loads for Buildings and Other Structures
American Society of Civil Engineers
1801 Alexander Bell Drive
Reston, VA 20191
(800) 548-2723
http://www.asce.org/

NOTE: Use UFC 3-301-01, Structural Engineering, for reference on some frost depth and ground snow load values.

2-2.7 Suggestions for Use.

The dry bulb, wet bulb, and humidity ratio values in Figure 2-1 are peak load conditions and are used for sizing mechanical equipment. Design guidance determines the frequency of occurrence design is to be based upon.

2-2.7.1 Dry Bulb Temperature.

The 0.4% dry bulb temperature value is seldom used for sizing conventional comfort control systems but is sometimes appropriate for mission-critical systems where equipment failure due to high heat would be unacceptable. Using the 0.4% value for equipment sizing requires that the engineer consider its operation at less-than-peak design conditions. In the past, oversized cooling equipment has been incapable of modulating during the more common range of operating conditions, yielding comfort control problems. Also, over-sized equipment cycles on and off more frequently, increasing maintenance costs and failing to remove enough moisture to maintain humidity control.

2-2.7.1.1 Design for Extreme Conditions.

Similar special considerations apply to the extreme low dry bulb temperature. Heating equipment designed for extreme conditions must be evaluated carefully to ensure that it will modulate properly to maintain comfort at less extreme outdoor temperatures that occur in 99.6% of the hours during the year.

2-2.7.1.2 Design of Humidity Control Systems.

The mean coincident value for humidity at the 0.4% peak dry bulb temperature is not the highest moisture value and must not be used for design of humidity control systems. The mean coincident value is the arithmetic average of all the moisture levels that occur
when the dry bulb temperature is high; however, the highest moisture values typically occur when the dry bulb temperatures are lower.

### 2-2.7.2 Wet Bulb Temperature.

High wet bulb temperature is used for sizing cooling towers and other evaporative equipment.

### 2-2.7.3 Peak Humidity Ratio.

Peak humidity ratio is used for sizing dehumidification systems. Peak moisture condition usually represents a higher enthalpy (total heat) than peak dry bulb condition. Consequently, engineers use the peak moisture condition to cross-check operation of a system that may be primarily intended to control temperature.

### 2-2.7.4 Coincident Wind Speed.

Coincident wind speed allows the engineer to accurately estimate latent loads due to infiltration of humid air in the summer and of dry air in the winter.

NOTE: The same precautions that apply to heating and cooling equipment also apply to dehumidification and humidification systems. Oversized equipment may not control properly under typical operating conditions without special attention from the engineer.

### 2-3 DATA SET PAGE 2: AVERAGE ANNUAL CLIMATE.

Figure 2-2 is an example of Data Set Page 2, a graph summarizing the site’s average annual climate.

#### 2-3.1 Explanation of Graph.

The graph on Data Set Page 2 shows the site’s monthly mean temperature, dew point, and precipitation. The bar graph representing precipitation uses the scale on the right side of the chart (inches or centimeters). Lines of temperature and dew point use the scale on the left side of the chart (degrees Fahrenheit or Celsius). These charts have fixed maximum and minimum values on their axes for easy comparison between different sites. The precipitation chart is capped at a maximum of 45 centimeters (15 inches) per month. A few sites may exceed this value, but to keep the graph readable, a fixed maximum value was used. For a number of sites, no accurate precipitation data was available. In those cases, no bars appear on the chart.

#### 2-3.2 Suggestions for Use.

##### 2-3.2.1 Comparisons.

The Data Set Page 2 graph displays the average behavior of weather over a single year. An architect can compare rainfall patterns at one station with another and also the relative importance of water resistance for the exterior envelope. An engineer can compare the temperature and moisture patterns to understand the relative importance of sensible heat loads rather than latent loads at this location.
2-3.2.2 Seasonal Variations.

With averages displayed by month, it is relatively easy to comprehend seasonal variation of each variable, and also to understand which specific months are likely to be hot or cold, humid or dry, or have high precipitation. This can be helpful for mission planning, as well as for planning construction and building operation.

NOTE: This graph displays averages, not design or extreme values. Data shown should not be used to determine equipment capacities or thermal characteristics of building envelopes.
Figure 2-2 Sample Data Set Page 2

Average Annual Climate

- Precipitation (inches)
- Temperature (°F)

Legend:
- Green: Mean Precipitation
- Red: Mean Temperature
- Blue: Mean Dewpoint

SCOTT AFB MID AMERICA IL
Page (2 of 18)
2-4 DATA SET PAGE 3: 30-YEAR PSYCHROMETRIC SUMMARY.

Figure 2-3 is an example of Data Set Page 3, a graph summarizing the site’s psychrometric data.

2-4.1 Explanation of Graph.

2-4.1.1 Joint-Frequency Table.

The graph displays the joint cumulative percent frequency of temperature and humidity ratio. Hourly observations are grouped into bins of 5 Fahrenheit degrees and 10 grains per pound (gr/lb) (or 3 Celsius degrees and 1.5 grams per kilogram [g/kg]), centered on each value of temperature or humidity ratio. For example, the 70 °F temperature bin collects all observations between 67.5 °F and 72.5 °F. The bin is depicted as a gridline on the chart; the vertical lines represent the temperature bins and the horizontal lines represent the humidity ratio bins. The intersection of temperature and humidity ratio lines represent a further subdivision of the observations into groups meeting both temperature and humidity ratio criteria. For example, the intersection of the 70 °F bin line and the 40 gr/lb bin line represent the observations when temperature was between 67.5 °F and 72.4 °F and the humidity ratio was between 35 gr/lb and 44 gr/lb. Thus, a joint-frequency table is created for all temperature and humidity ratio bin combinations.

NOTE: The psychrometric graph is intended as a visual tool only. Its purpose is to allow a quick visual comparison between climates at different locations. Extrapolation of data directly from the graph is not advised due to the approximate plotting routine used to generate the graph from the binned data. This is evident where values of humidity appear past their saturation point. This discrepancy between the actual data and the graph is the result of the plotting routine used to generate the graph and not from errors in the original hourly data used to create the binned summary.

2-4.1.2 Contours.

The contours on this chart represent the areas containing 99%, 97.5%, 95%, 80%, and 50% of all observations (cumulative percent frequency or percentiles). The contours are centered on the most frequently occurring bins (50% contour), spreading outward until almost all observations (99%) are grouped. Contours are defined by calculating a percent frequency for each bin (relative to the others), and then accumulating these percent frequencies (from most frequent to least frequent) until the 50% value is passed, and thus the first set of bins is grouped. The accumulating continues until the 80% value is passed, and the second group of bins is grouped. This process continues until the 95%, 97.5%, and 99% values are passed.

2-4.1.3 Least Frequent (Most Extreme) Bins.

Consequently, the least frequent (most extreme) bins, which when accumulated amount to less than 1 percent of the total observations, are outside of the 99% contour. Any bins outside the 99% contour thus have either not occurred, or have occurred so infrequently that they should not be taken into consideration for sizing equipment.
Figure 2-3 Sample Data Set Page 3

Long Term Psychrometric Summary

Temperature (F)  
Humidity Ratio (g/lb)

Percent of observations: 99% 92.5% 95% 80% 50%

SCOTT AFB MIDAMERICA IL  Page (3 of 18)
2-4.2 Suggestions for Use.

2-4.2.1 Most Common Temperature and Moisture Conditions.

The Data Set Page 3 graph displays the long-term history of temperature and moisture at each station (a total of 262,800 hourly observations if the POR is 30 years and if the data is complete over that period). The engineer can use this graph to ascertain the most common temperature and moisture conditions that will be encountered over the operating life of the mechanical equipment.

2-4.2.2 Ensure Modulation and ControlCapability.

It is often useful to calculate the behavior of the proposed system at “most common” conditions and assess these calculations in addition to the traditional peak design calculations. This will help ensure that the selected equipment and controls are capable of modulation and control at all points of operation rather than simply at extreme conditions.

2-5 DATA SET PAGE 4: PSYCHROMETRIC DISPLAY OF DESIGN VALUES.

Figure 2-4 is an example of Data Set Page 4, a psychometric display of the site’s design values.

2-5.1 Saturation Curve.

Similar to Data Set Page 3, this chart depicts the saturation curve (when RH = 100%) along with peak design values. The design values are calculated as in the table on Data Set Page 1 (Figure 2-1), but this chart shows their relationships graphically, depicting their position relative to each other and relative to the saturation curve.

2-5.2 Observations.

Above and to the left of the saturation curve, RH would be greater than 100% (not possible). The area below and to the right of the curve (including the points on the curve itself) represent the area where RH is less than or equal to 100%, and thus where all observations occur. Note that since the humidity ratio is a function of pressure, and pressure varies with elevation, different sites will have different saturation curves.

2-5.3 Scatter Plot.

The dry bulb temperature is the horizontal coordinate on this scatter plot, and the humidity ratio is the vertical coordinate. Peak design values are depicted by the red square (1.0% Temperature [dry bulb]), the green circle (1.0% Humidity Ratio), and the blue diamond (99% Temperature [dry bulb]).

2-5.4 Table.
The table below the chart shows the exact values of 99% dry bulb temperature, 1.0% humidity ratio, and 1.0% dry bulb temperature, along with calculated values of enthalpy, mean coincident wet bulb temperature, and humidity ratio (as applicable). The value of enthalpy coincident to each temperature/humidity ratio is created using the psychrometric functions provided by the Linric Company, Bedford, New Hampshire. The dry bulb temperature and humidity ratio are used to calculate enthalpy using the Linric algorithms.
Figure 2-4 Sample Data Set Page 4

Psychrometric Summary of Peak Design Values

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<th></th>
<th>(°C)</th>
<th>MCDB (°F)</th>
<th>MCWB (°F)</th>
<th>MCDP (°F)</th>
<th>MCHR (°F)</th>
<th>Enthalpy (Btu/lb)</th>
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</thead>
<tbody>
<tr>
<td>1.0% Dry Bulb</td>
<td>93.0</td>
<td>77</td>
<td>116.0</td>
<td>-40.6</td>
<td></td>
<td></td>
</tr>
<tr>
<td>99.0% Dry Bulb</td>
<td>11.0</td>
<td></td>
<td></td>
<td>7.0</td>
<td>1.6</td>
<td></td>
</tr>
<tr>
<td>1.0% Humidity Ratio</td>
<td>141.0</td>
<td>83.0</td>
<td>78.5</td>
<td>76.7</td>
<td>-42.1</td>
<td></td>
</tr>
</tbody>
</table>

SCOTT AFB MID/AMERICA II  Page (4 of 18)
2-6  DATA SET PAGES 5 THROUGH 9: TEMPERATURE BIN DATA.

Figures 2-5 through 2-9 are examples of Data Set Pages 5 through 9, respectively. These tables show the number of hours that temperatures occur in 5 Fahrenheit degree (3 Celsius degree) bins of specific 8-hour daily periods during a given month. The 8-hour periods are based upon a 24-hour clock and displayed in Local Standard Time (LST). For each month, the number of observations for each temperature bin during each of the specific 8-hour periods of the day appear in a column under the specific Hour Group (LST). The total number of observations (hours) in each temperature bin is displayed in the “Total Obs” column for the month. The mean coincident wet bulb temperature is the mean value of all those wet bulb temperatures that occur coincidentally with the dry bulb temperatures in the particular 5° temperature bin. At the upper, or warmer, end of the mean coincident wet bulb distribution, the values occasionally reverse their trend because the highest wet bulb temperatures do not necessarily occur with the highest dry bulb temperatures. There are 13 such tables, one for each month and one representing the overall annual summary (Data Set Page 9).

2-6.1  Suggestions for Use.

Binned summaries are used by many different technical disciplines for different purposes. They are useful in making informal estimates of energy consumption by cooling and heating equipment, and for gaining a general understanding of patterns of temperature and moisture at different times of the day, month, and year.

NOTE: Do not use these binned summaries to calculate design moisture loads.

2-6.2  Comments.

These particular binned summaries are based on the dry bulb temperature. After each observation has been placed into a dry bulb bin, the average humidity ratio is calculated for all observations in each bin. Consequently, dry bulb bins underestimate the magnitude of dehumidification and humidification loads because the averaging calculation “flattens” the peaks and valleys of humidity ratios. The amount of the underestimation varies according to the intended humidity control level.
**Figure 2-5 Sample Data Set Page 5**

### Dry-Bulb Temperature Hours For An Average Year

<table>
<thead>
<tr>
<th>Temperature Range (°F)</th>
<th>January</th>
<th>February</th>
<th>March</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>01 To 08 LST</td>
<td>09 To 16 LST</td>
<td>17 To 00 LST</td>
</tr>
<tr>
<td>105/109</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>100/104</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>95/94</td>
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</tr>
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<td>5</td>
</tr>
<tr>
<td>75/79</td>
<td>0</td>
<td>0</td>
<td>1</td>
</tr>
<tr>
<td>70/74</td>
<td>1</td>
<td>1</td>
<td>7</td>
</tr>
<tr>
<td>65/69</td>
<td>0</td>
<td>4</td>
<td>1</td>
</tr>
<tr>
<td>60/64</td>
<td>2</td>
<td>10</td>
<td>2</td>
</tr>
<tr>
<td>55/59</td>
<td>4</td>
<td>14</td>
<td>2</td>
</tr>
<tr>
<td>50/54</td>
<td>7</td>
<td>21</td>
<td>1</td>
</tr>
<tr>
<td>45/49</td>
<td>14</td>
<td>36</td>
<td>4</td>
</tr>
<tr>
<td>40/44</td>
<td>19</td>
<td>38</td>
<td>4</td>
</tr>
<tr>
<td>35/39</td>
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<td>4</td>
</tr>
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<td>30/34</td>
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<td>40</td>
<td>4</td>
</tr>
<tr>
<td>25/29</td>
<td>43</td>
<td>26</td>
<td>4</td>
</tr>
<tr>
<td>20/24</td>
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<td>4</td>
</tr>
<tr>
<td>15/19</td>
<td>15</td>
<td>10</td>
<td>1</td>
</tr>
<tr>
<td>10/14</td>
<td>17</td>
<td>9</td>
<td>1</td>
</tr>
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<td>5/9</td>
<td>6</td>
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<td>1</td>
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<td>-10/-6</td>
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</tr>
<tr>
<td>-20/-16</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
</tbody>
</table>

Caution: This summary reflects the typical distribution of temperature in a typical year. It does not reflect the typical moisture distribution. Because wet bulb temperatures are averaged, this summary understates the annual moisture load. For accurate moisture load data, see the long-term humidity summary and the ventilation and infiltration load pages in this manual.
Figure 2-6 Sample Data Set Page 6

Dry-Bulb Temperature Hours For An Average Year

<table>
<thead>
<tr>
<th>Temperature Range (°F)</th>
<th>April</th>
<th>May</th>
<th>June</th>
</tr>
</thead>
<tbody>
<tr>
<td>105/109</td>
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<td>71.3</td>
</tr>
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<td>95/99</td>
<td>0</td>
<td>0</td>
<td>75.5</td>
</tr>
<tr>
<td>90/94</td>
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<td>1</td>
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</tr>
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<td>85/89</td>
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<td>5</td>
<td>68.6</td>
</tr>
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<td>80/84</td>
<td>4</td>
<td>18</td>
<td>66.1</td>
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<td>75/79</td>
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</tr>
<tr>
<td>70/74</td>
<td>6</td>
<td>23</td>
<td>60.7</td>
</tr>
<tr>
<td>65/69</td>
<td>12</td>
<td>23</td>
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<td>59</td>
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<td>21.8</td>
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</tbody>
</table>

Caution: This summary reflects the typical distribution of temperature in a typical year. It does not reflect the typical moisture distribution. Because wet bulb temperatures are averaged, this summary understates the annual moisture load.
For accurate moisture load data, see the long-term humidity summary and the ventilation and infiltration load pages in this manual.
## Dry-Bulb Temperature Hours For An Average Year

<table>
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<tr>
<th>Temperature Range (°F)</th>
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<th>September</th>
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<td>17 to 00 LST</td>
</tr>
<tr>
<td>105/109</td>
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<td>2</td>
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<td>2</td>
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<tr>
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<td>21</td>
</tr>
<tr>
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<td>59</td>
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</tr>
<tr>
<td>85/89</td>
<td>18</td>
<td>63</td>
<td>56</td>
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</tr>
<tr>
<td>75/79</td>
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</tr>
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<td>65</td>
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<td>14</td>
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<td>5/9</td>
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</tr>
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<tr>
<td>-20/-16</td>
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</tr>
</tbody>
</table>

Caution: This summary reflects the typical distribution of temperature in a typical year. It does not reflect the typical moisture distribution. Because wet bulb temperatures are averaged, this summary understates the annual moisture load. For accurate moisture load data, see the long-term humidity summary and the ventilation and infiltration load pages in this manual.
## Dry-Bulb Temperature Hours For An Average Year

<table>
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<th>Temperature Range (°F)</th>
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<th>November</th>
<th>December</th>
</tr>
</thead>
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<td></td>
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<td>09 To 16 LST</td>
<td>17 to 00 LST</td>
</tr>
<tr>
<td>105/109</td>
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<td></td>
<td></td>
</tr>
<tr>
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<td>71.9</td>
</tr>
<tr>
<td>85/89</td>
<td>5</td>
<td>0</td>
<td>5</td>
</tr>
<tr>
<td>80/84</td>
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<td>1</td>
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</tr>
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<td>34</td>
<td>24</td>
</tr>
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<td>39</td>
</tr>
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<td>55/59</td>
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<td>50/54</td>
<td>47</td>
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</tr>
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<td>15/19</td>
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</tr>
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<td>1</td>
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<tr>
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</tr>
<tr>
<td>-15/-11</td>
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<td>0</td>
<td>0</td>
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</tbody>
</table>

Caution: This summary reflects the typical distribution of temperature in a typical year. It does not reflect the typical moisture distribution. Because wet bulb temperatures are averaged, this summary understates the annual moisture load. For accurate moisture load data, see the long-term humidity summary and the ventilation and infiltration load pages in this manual.
**Dry-Bulb Temperature Hours For An Average Year**

<table>
<thead>
<tr>
<th>Temperature Range (°F)</th>
<th>01 To 08 LST</th>
<th>09 To 16 LST</th>
<th>17 To 00 LST</th>
<th>Total Obs</th>
<th>MCBW</th>
</tr>
</thead>
<tbody>
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<td>0</td>
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<td>76.5</td>
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</tr>
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<td></td>
</tr>
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<td>187</td>
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<td>73.7</td>
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<td>185</td>
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<td>-15.5</td>
</tr>
</tbody>
</table>

Caution: This summary reflects the typical distribution of temperature in a typical year. It does not reflect the typical moisture distribution. Because wet bulb temperatures are averaged, this summary understates the annual moisture load. For accurate moisture load data, see the long-term humidity summary and the ventilation and infiltration load pages in this manual.
2-7 DATA SET PAGE 10: ANNUAL TEMPERATURE SUMMARY.

Figure 2-10 is an example of Data Set Page 10. This chart shows a week-by-week summary of dry bulb temperatures for the given site. The observations are grouped into 7-day periods (approximate calendar weeks). For example, observations from January 1 through 7 from all years are grouped, observations from January 8 through 14 from all years are grouped, and so on, overlapping the end of one month and beginning of the next month where necessary. The following statistics are shown for each of the 7-day periods:

- **1% Dry Bulb Temp** is the dry bulb temperature that is exceeded 1% of the time during that calendar week.
- **MCWB (1% Dry Bulb)** is the mean of wet bulb temperatures coincident with 1% dry bulb temperatures during the same week.
- **Mean Max Temp** is the daily maximum dry bulb temperature, averaged by week over the POR.
- **Mean Min Temp** is the daily minimum dry bulb temperature, averaged by week over the POR.
- **99% Min Dry Bulb Temp** is the daily dry bulb temperature that is at or above this value 99% of the time, or below this value 1% of the time.

**NOTE:** The information in this chart is calculated on a weekly basis; information on a climate summary (Data Set Page 1) is calculated on an annual basis.

2-7.1 Suggestions for Use.

The weekly 1% and 99% temperatures are useful for understanding the probable temperature extremes that can occur during a given week of the year. The weekly dry bulb temperatures are useful for understanding the change of seasons at a given location. The display is helpful for mission planning and construction project planning.

2-7.2 Special Considerations.

2-7.2.1 Designers.

The values displayed here are based on the 30-year record. It is important that designers not base equipment selection on the “highest” or “lowest” recorded temperature at the station. That error would result in selecting equipment extremely costly to install, which would operate inefficiently for all but the very hottest or coldest single hour in 30 years. See the Design Criteria Data section on Sample Data Set Page 1 (see Figure 2-1) in this document for appropriate maximum and minimum temperatures for sizing equipment.

2-7.2.2 Construction and Operation Planners.

The mean maximum and minimum temperatures shown for each week seldom occur in the same year. Keep in mind that these are mean values that are useful for
understanding the typical range of temperatures in a given week. The difference does not represent the actual day-night temperature swing in a given week.
Figure 2-10 Sample Data Set Page 10

Annual Summary of Temperatures

Temperature (°F)

Month

1% Dry Bulb Temp
Mean Min Temp
Mean Max Temp
MCWB (1% Dry Bulb)
99% Min Dry Bulb Temp

SCOTT AFB MIDAMERICA IL Page (10 of 18)
2-8 DATA SET PAGE 11: ANNUAL HUMIDITY SUMMARY.

Figure 2-11 is an example of Data Set Page 11. Similar to the annual temperature summary (see Sample Data Set Page 10, Figure 2-10), this chart depicts mean maximum and minimum values of humidity ratio, plus the 1% maximum humidity ratio, along with its mean coincident dry bulb temperature, summarized by calendar week. The chart uses two vertical axes: on the left are the humidity ratio values and on the right is a temperature scale for the mean coincident dry bulb temperature.

2-8.1 Suggestions for Use.

Weekly humidity ratios are useful for understanding the change of seasons at a given location and the probable high and low moisture levels during a given week of the year. The display is helpful for planning humidity-controlled storage projects and for understanding factors contributing to atmospheric corrosion. Humidity also affects the deterioration rate of building materials and the weathering of military equipment and structures exposed to the elements.

2-8.2 Special Considerations.

2-8.2.1 Designers.

The values displayed here are based on the 30-year record. It is important that designers not base equipment selection on the “highest” or “lowest” recorded humidity at the station. That error would result in selecting oversized equipment, which would increase costs and might result in control problems at other than extreme conditions. Use design values on Data Set Page 1 (Figure 2-1) for equipment sizing.

2-8.2.2 Construction and Operation Planners.

The high and low humidity ratios shown for each week seldom occur in the same year. Keep in mind that these are mean values that are useful for understanding the typical range of humidity ratio in a given week. The difference does not represent the actual day-night humidity ratio swing in a given week.

2-9 DATA SET PAGE 12: ANNUAL DRY BULB TEMPERATURE AND HUMIDITY SUMMARY TABLES.

Figure 2-12 is an example of Data Set Page 12. Data Set Page 12 consists of tables containing the values used to plot the charts on Data Set Page 10 and Data Set Page 11. The left half of the table uses Data Set Page 10 and the right half uses Data Set Page 11.
Figure 2-11 Sample Data Set Page 11

Long Term Humidity and Dry Bulb Temperature Summary

SCOTT AFB MIDAMERICA IL   Page (11 of 18)
Figure 2-12 Sample Data Set Page 12

<table>
<thead>
<tr>
<th>Week Ending</th>
<th>1.0% Temp (°F)</th>
<th>MCWB@1% Temp (°F)</th>
<th>Mean Max Temp (°F)</th>
<th>Mean Min Temp (°F)</th>
<th>99% Temp (°F)</th>
<th>1.0% HR (gr/lb)</th>
<th>MCDB@1% HR (°F)</th>
<th>Mean Max HR (gr/lb)</th>
<th>Mean Min HR (gr/lb)</th>
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</thead>
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<tr>
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<td>39.2</td>
<td>23.3</td>
<td>3</td>
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<td>618</td>
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</tr>
</tbody>
</table>
Figure 2-13 is an example of Data Set Page 13. Data Set Page 13 consists of charts summarizing a site’s mean heating and cooling degree days.

2-10.1 Explanation of Charts.

2-10.1.1 Calculation of Cooling Degree-Days.

Cooling degree-days are derived by multiplying the number of hours that the outdoor temperature is above the base temperature of 65 °F (18 °C) times the number of degrees of that temperature difference. For example, if 1 hour was observed at a temperature of 78 °F, that observation adds 13 degree-hours to the annual total. The sum of the degree-hours is divided by 24 to yield degree-days.

2-10.1.2 Calculation of Heating Degree-Days.

Heating degree-days are calculated similarly, against the base temperature of 65 °F, so a 1-hour outside temperature observation of 62 °F adds 3 degree-hours to the annual total. Heating degree-days are summed separately from the cooling degree-days. Heating and Cooling degree-hours do not cancel each other out, since both heating and cooling conditions may occur over the course of a given day.

2-10.1.3 Alternate Cooling Degree-Days Calculation.

A separate file has been added to the 14 WS Web site to include the cooling degree-days based upon a base temperature of 50 °F. This file is located on the Engineering Weather Data page under the Standard EWD Package file. This data is intended to allow selection of the proper Building Envelope Requirements table from within ASHRAE/IESNA Standard 90.1 of 2013 for energy conservation design. The cooling degree-days based on 65 °F tabulated and graphed here are historically used to estimate loads as suggested in paragraph 2-10.2 below.

2-10.2 Suggestions for Use.
Degree-days are used to estimate the sensible heat and sensible cooling loads on the building envelope. Degree-day loads can be used to estimate the annual energy consumption of a building, provided that the loads from ventilation and infiltration air are also considered (see paragraph 2-11).
Figure 2-13 Sample Data Set Page 13

Degree Days, Heating and Cooling
(Base 65 F) & Cooling (Base 50F)

<table>
<thead>
<tr>
<th>Month</th>
<th>Mean Cooling Degree Days</th>
<th>Mean Heating Degree Days</th>
</tr>
</thead>
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<td></td>
<td></td>
<td>(°F)</td>
</tr>
<tr>
<td></td>
<td>Base 50</td>
<td>Base 65</td>
</tr>
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<td>1.1</td>
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2-11 DATA SET PAGE 14: VENTILATION AND INFILTRATION LOADS.

Figure 2-14 is an example of Data Set Page 14. Data Set Page 14 consists of a graph and table that display the independent loads imposed by heating, cooling, humidifying, and dehumidifying outside air as it is brought into a building. The calculation assumes that air inside the building is maintained at conditions between 68 °F (20 °C)/30% RH and 75 °F (24 °C)/60% RH. For the purposes of these calculations, when the outside air is within that range of temperature and moisture, any incoming air is assumed not to impose any load.

These values are calculated with the methodology used to calculate the annual VCLI on Data Set Page One, except that values on this page are computed by month and the result is displayed as British thermal units per cubic foot per minute (Btu/CFM) rather than as ton-hours per CFM per year. The heating and humidifying loads are shown as negative values. Cooling and dehumidifying loads are displayed as positive values.

2-11.1 Suggestions for Use.

Bringing fresh ventilation air into a building or allowing air to infiltrate into buildings through cracks imposes heating, cooling, dehumidification, and humidification loads on the mechanical system. The information on this data set page helps the architect, engineers, and operating personnel understand the nature and magnitude of those loads on an annual basis. It also shows how the loads vary from month to month throughout the year.

2-11.2 Comments.

These calculations are based on the load created when 1 cubic foot of outside air is brought into the building each minute. The results of the calculation include the moisture load or deficit, and the sensible heat load or deficit created by that cubic foot of air during each month of the year. Note that most months have both a load and a deficit for temperature and moisture. The monthly deficit and load do not “cancel” from the perspective of the mechanical system, because temperature and moisture loads will often occur at different times of the day.

NOTE: The values displayed here assume that the inside air is maintained between 68 °F/30% RH and 75 °F/60% RH. If the inside conditions are held in a different range of temperature or moisture, the loads will be different. For example, in calculating loads for humidity-controlled but unheated storage, the loads vary according to the change in both temperature and humidity, since the inside temperature varies but the inside humidity is held constant. For estimating loads in that or similar applications, the engineer may obtain better results by using the average maximum weekly humidity data shown on Data Set Pages 11 and 12 (Figures 2-11 and 2-12).
Figure 2-14 Sample Data Set Page 14

Average Ventilation and Infiltration Loads
(Outside Air vs 75°F, 60% RH summer; 68°F, 30% RH winter)

<table>
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<th>Average Sensible Heating Load (Btu/ft²)</th>
<th>Average Latent Cooling (Drying) Load (Btu/ft²)</th>
<th>Average Latent Heating (Humidifying) Load (Btu/ft²)</th>
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2-12 DATA SET PAGES 15 AND 16: SOLAR RADIATION DATA.

Figures 2-15 and 2-16 are samples of Data Set Page 15 and Data Set Page 16, respectively.

2-12.1 Explanation of Charts.

2-12.1.1 Data Source.

This data is reproduced courtesy of the National Renewable Energy Laboratory (NREL). The data were first published in the NREL’s Solar Radiation Data Manual for Buildings (1995). The user should refer to that publication for a complete description of how to use this data. The manual can be accessed online at http://www.osti.gov/bridge by searching for “NREL/TP--463-7904.”

2-12.1.2 Site Location.

The site used in each station record is the nearest NREL-published site available within a 1.5° latitude radius from the requested location. Consequently, some sites may be several miles away, and in some cases, the NREL location may be in a neighboring state. Use caution when the nearest site available is not in the same city as the requested location, since significant differences in cloud climatology can exist over short distances.

2-12.1.3 Site Availability.

When this document was prepared, the only sites available from NREL were Puerto Rico, Guam, and the 50 states. For locations where solar radiation data is not available, Data Set Pages 15 and 16 are blank. For these locations, users may wish to contact NREL directly to obtain advice concerning data not published in the NREL solar radiation data manual.

2-12.2 Suggestions for Use.

The solar data presented here can be used for calculating solar radiation cooling loads on building envelopes, and also for estimating the value of solar illumination for daylighting calculations. Again, the user should refer to the Solar Radiation Data Manual for Buildings for a complete description of how to use this data.

NOTE: The data source for the NREL reports comes from the National Solar Radiation Database—not the data set used to calculate peak design values and other monthly temperature and moisture data in this document. The two data sets will differ for many reasons, including different POR, measurement locations, sampling methodology and frequency, and differences in calculation methodology. Consequently, the user should expect differences in degree-days, minimum and maximum temperatures, and humidity values between this data and that calculated by the 14 WS. For design criteria, use the temperature and moisture values presented on the Design Criteria Data section of Data Set Page 1 (see Figure 2-1) of this document. These were calculated more recently and
used a longer POR. Also, they are taken from records at DoD locations rather than from civilian locations near—but not always identical to—the military data collection points.
### Average Annual Solar Radiation - Closest Available Site
Source: National Renewable Energy Laboratory, Golden CO, 1995

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#### AVERAGE INCIDENT SOLAR RADIATION (Btu/sq.ft/day) Percentage Uncertainty = 9%

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SCOTT AFB MIDAMERICA IL
### Average Annual Solar Radiation - Nearest Available Site
Source: National Renewable Energy Laboratory, Golden CO, 1995

**Average Transmitted Solar Radiation (W/m²) for Double Glazing**
Percentage Uncertainty = 9

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**Average Incident Illuminance (lx) for Mostly Clear and Mostly Cloudy Conditions**
Percentage Uncertainty = 9

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**Percentage Uncertainty = 9**
Figure 2-17 Sample Data Set Page 17

Wind Summary - December, January, and February

Wind Summary - March, April, and May
Figure 2-18 Sample Data Set Page 18

Wind Summary - June, July, and August

Wind Summary - September, October, and November
2-13 DATA SET PAGES 17 AND 18: WIND SUMMARY.

Figures 2-17 and 2-18 are samples of Data Set Page 17 and Data Set Page 18, respectively.

2-13.1 Explanation of Charts.

2-13.1.1 Depiction.

These charts depict the frequency of different wind direction and wind speed combinations. The observations are binned into 36 compass directions and 5 speed categories (1 to 5 knots, 6 to 14 knots, 15 to 24 knots, 25 to 34 knots, and greater than 34 knots). The frequency of direction and the tick marks indicate that values lie along each “spoke” of the wind chart. The wind speed bins for each direction are color coded by the legend at the bottom of the chart.

2-13.1.2 Percent Frequency.

To determine the percent frequency of a particular wind direction, look for the tick mark bounding the outer edge of a colored (wind speed) area. In the case of the first wind speed bin (1 to 5 knots), the percent frequency is simply the value of the tick mark on the outer edge of the 1 to 5 knot region. For the higher speed bins (6 to 14 knots or greater), subtract the earlier spoke values from the value shown to get the frequency for the speed bin in question.

2-13.1.3 Total Percent Frequency.

The values for percent frequency have been summed by direction, so to determine the total percent frequency for all speeds from a particular direction, look up the tick mark (or interpolated value) bounding the outermost colored area along that spoke. That tick mark represents the total percent frequency of wind from that direction.

2-13.1.4 Calm Conditions.

Since the calm condition has no direction, the percent occurrence of calm conditions is displayed at the center of the chart.

2-13.2 Wind Summary Chart Example.

The wind summary charts are prepared by 3-month seasons, over all hours (e.g., December, January, February for northern hemisphere winter or southern hemisphere summer; March, April, May for northern hemisphere spring or southern hemisphere fall). See the December through February sample wind summary chart in Figure 2-17 for an example of determining percent frequencies.

2-13.2.1 December through February.

From the December through February sample wind summary chart, the percent frequency of wind between 1 to 5 knots and from the north (N) is about 1%. The percent frequency of wind between 6 to 14 knots and from the south (S) is about 3% (~4.25%
minus ~1.25%). The percent frequency of all wind speeds from the south (S) is about 5%. The percent frequency of all wind directions from the west through north (270° - 360°) is about 35% (2% + 2.75% + 3.875% + 4.5% + 4.5% + 4.25% + 3.875% + 3.25% + 3% + 3%, respectively – all values approximated). It is easy to determine that wind speeds greater than 34 knots almost never occur (or are such a small frequency from any direction) because the colored area (yellow) is not shown or is indistinguishable because it is extremely small.

2-13.2.2 Calm Wind.

The percent of time the wind is calm is indicated in the center of the chart—in this case, 8.1%. When the outermost value from each of the 36 directions are summed and added to the percent calm, the result is 100% (allowing for rounding). Occurrences of variable wind direction are omitted from the sample before computing percent frequency by direction.

2-13.3 Suggestions for Use.

Knowing the probable wind speed and direction in a particular month can be helpful in construction and mission planning as well as in designing structures that experience severe wind-driven rain or drifting snow. Engineers designing outside air intake and building exhaust vents for heating and air conditioning systems can use these data to minimize the potential for cross-contamination between supply and exhaust air streams. Also, when drifting snow accumulation on roofs is likely, the information on these data set pages can be helpful for locating inlet and exhaust ducts so they are less likely to be obstructed by snowdrifts.

NOTE: The wind currents around any building are strongly affected by the geometry of the building and the topography of the site as well as those of any surrounding buildings. The wind data used for these wind summaries are typical of flat and open airfields where there are no obstructions near the observation point.
APPENDIX A REFERENCES

AMERICAN SOCIETY OF CIVIL ENGINEERS
http://www.asce.org/

AMERICAN SOCIETY OF HEATING, REFRIGERATING AND AIR-CONDITIONING ENGINEERS (ASHRAE)
http://www.ashrae.org/

INTERNATIONAL CODE COUNCIL
http://www.iccsafe.org/
International Plumbing Code, 2012

NATIONAL GROUND WATER RESEARCH AND EDUCATIONAL FOUNDATION
http://www.ngwa.org/

NATIONAL RENEWABLE ENERGY LABORATORY
http://www.osti.gov/bridge
Solar Radiation Data Manual for Buildings, 1995

UNITED STATES DEPARTMENT OF DEFENSE
http://www.dtic.mil/whs/directives/
DoD Directive 4715.21, Climate Change Adaptation and Resilience, 14 January 2016

UNIFIED FACILITIES CRITERIA
http://www.wbdg.org/ccb/browse_cat.php?o=29&c=4
UFC 1-200-01, DoD Building Code (General Building Requirements)
UFC 3-301-01, Structural Engineering
APPENDIX B BEST PRACTICES

B-1 BEST PRACTICES.

No best practices are documented at this time.
## APPENDIX C GLOSSARY

### C-1 ACRONYMS

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<th>Abbreviation</th>
<th>Definition</th>
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<td>Army Air Field</td>
<td>British thermal units</td>
</tr>
<tr>
<td>AB</td>
<td>Air Base</td>
<td>British thermal units per cubic foot per minute</td>
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<td>British thermal units per pound of air (enthalpy)</td>
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<td>British thermal units per square foot per day (solar radiation)</td>
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<td>Fahrenheit</td>
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<tr>
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<td>Air Reserve Base</td>
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g/kg  Grams per kilogram (humidity ratio, grams of water vapor per kilogram of air)
in. Hg  Inches of mercury (atmospheric pressure)
in.  Inches (frost depth)
in./hr  Inches per hour (rain rate)
klux-hr  Thousands of lux-hours (average incident illuminance)
lb/ft²  pounds per square foot (snow load)
LST  Local Standard Time
MCAS  Marine Corps air station
MCB  Marine Corps base
MC Dewpt  Mean Coincident Dewpoint
MCDB  Mean of dry bulb temperatures
MCHR  Mean Coincident Humidity Ratio
MCWB  Mean of wet bulb temperatures
mph  Miles per hour (wind speed)
NAS  Naval Air Station
NAF  Naval Air Facility
NAVFAC  Naval Facilities Engineering Command
NCDC  National Climatic Data Center
NRC  Naval Reserve Center
NREL  National Renewable Energy Laboratory
NS  Naval Station
NSA  Naval Support Activity
POR  Period of record
RH  Relative humidity
ton-hr/ft³/yr  Ton-hours of load per cubic foot per minute per year (Btu÷12,000)
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APPENDIX D SAMPLE 14 WS SUPPORT ASSISTANCE REQUEST (SAR) FORM

14WS SUPPORT ASSISTANCE REQUEST (SAR)

SUBJECT

CONTACT INFORMATION

RANK/TITLE
FULL NAME

TELEPHONE NUMBER
E-MAIL

ORGANIZATION

ORGANIZATION TYPE:

Are you Meteorological or Oceanographic Personnel?
Are you a part of the Air Force Weather community?

STATION

LOCATION

REQUEST

When do you need your data?
Describe what you need, include specific locations, if applicable and all pertinent details:

Who will receive the information? What it will be used for? Include any tangible benefits or expected impacts. If classified, contact via classified email.

IF DOD CONTRACTOR

MILITARY POINT OF CONTACT

RANK/TITLE
FULL NAME

CONTACT TELEPHONE

CONTRACT NUMBER

14 WS FORM 1, DEC 12 (EF-V2)
PREVIOUS EDITIONS MAY BE USED
PAGE 1 OF 1 PAGES
APPENDIX E LIST OF AVAILABLE EWD SITES

E-1 REGULARLY UPDATED SITES.

Table E-1 is a list that consists of the Site Name, 4-letter Station ID, Latitude/Longitude, and Country for each Engineering Weather Data (EWD) site available at the 14th Weather Squadron. Note that the sites are regularly updated and the latest list should be retrieved at https://www.climate.af.mil.

Table E-1 List of Available EWD Sites

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